

# 1 Conservative formulation

Solve

$$T^{00}_{,0} = -T^{0i}_{,i} \quad (1)$$

$$T^{i0}_{,0} = -T^{ij}_{,j} \quad (2)$$

where

$$E \equiv T^{00} = \frac{4}{3}\rho\gamma^2 - \frac{1}{3}\rho = \frac{4}{3}\rho\gamma^2 (1 - 1/4\gamma^2) \quad (3)$$

$$T^{ij} = \frac{4}{3}\rho\gamma^2 u_i u_j + \frac{1}{3}\rho\delta_{ij} \quad (4)$$

Define

$$S_i \equiv T^{0i} = T^{i0} = \frac{4}{3}\rho\gamma^2 u_i \quad (5)$$

So  $\mathbf{u} = \epsilon_u \mathbf{S}$ , where  $\epsilon_u = 3/(4\rho\gamma^2) = (1 - 1/4\gamma^2)/E$ .  
using  $\mathbf{u}^2 = 1 - 1/\gamma^2$ ,

$$r \equiv (T^{i0}/T^{00})^2 = \frac{\gamma^4 - \gamma^2}{(\gamma^2 - 1/4)^2} \quad (6)$$

so

$$\gamma^4 - \gamma^2 - (\gamma^4 - \gamma^2/2 + 1/16)r = 0 \quad (7)$$

$$\gamma^4(1-r) - \gamma^2(1-r/2) - r/16 = 0 \quad (8)$$

$$\gamma^4 - \gamma^2(1-r/2)/(1-r) - r/[16(1-r)] = 0 \quad (9)$$

Solution for  $\gamma^2$  is

$$\gamma^2 = \frac{1-r/2}{2(1-r)} \pm \sqrt{\frac{(1-r/2)^2}{4(1-r)^2} + \frac{r}{16(1-r)}} \quad (10)$$

$$\gamma^2 = \frac{1-r/2}{2(1-r)} \pm \sqrt{\frac{(1-r/2)^2}{4(1-r)^2} + \frac{r-r^2}{16(1-r)^2}} \quad (11)$$

$$\gamma^2 = \frac{1}{2(1-r)} \left[ (1-r/2) \pm \sqrt{(1-r/2)^2 + \frac{r-r^2}{4}} \right] \quad (12)$$

$$\gamma^2 = \frac{1}{2(1-r)} \left[ (1-r/2) \pm \sqrt{1-r+r^2/4 + \frac{r-r^2}{4}} \right] \quad (13)$$

$$\gamma^2 = \frac{1}{2(1-r)} \left[ (1-r/2) \pm \sqrt{1-3r/4} \right] \quad (14)$$

## 2 Keep $c_s^2$

$$r \equiv (T^{i0}/T^{00})^2 = \frac{\gamma^4 - \gamma^2}{[\gamma^2 - c_s^2/(1+c_s^2)]^2} \quad (15)$$

$$\gamma^4 - 2\gamma^2 \frac{\frac{1}{2} - r \frac{c_s^2}{1+c_s^2}}{1-r} - \frac{r}{1-r} \left( \frac{c_s^2}{1+c_s^2} \right)^2 = 0 \quad (16)$$

$$\gamma^2 = \frac{\frac{1}{2} - r \frac{c_s^2}{1+c_s^2}}{1-r} + \sqrt{\left( \frac{\frac{1}{2} - r \frac{c_s^2}{1+c_s^2}}{1-r} \right)^2 + \frac{r}{1-r} \left( \frac{c_s^2}{1+c_s^2} \right)^2} \quad (17)$$

$$\gamma^2 = \frac{\frac{1}{2} - r \frac{c_s^2}{1+c_s^2}}{1-r} \left[ 1 + \sqrt{1 + \left( \frac{1-r}{\frac{1}{2} - r \frac{c_s^2}{1+c_s^2}} \right)^2 \frac{r}{1-r} \left( \frac{c_s^2}{1+c_s^2} \right)^2} \right] \quad (18)$$

$$\gamma^2 = \frac{\frac{1}{2} - r \frac{c_s^2}{1+c_s^2}}{1-r} \left[ 1 + \sqrt{1 + \frac{(1-r)r}{\left( \frac{1}{2} - r \frac{c_s^2}{1+c_s^2} \right)^2} \left( \frac{c_s^2}{1+c_s^2} \right)^2} \right] \quad (19)$$

$$\gamma^2 = \frac{1}{1-r} \left[ \frac{1}{2} - r \frac{c_s^2}{1+c_s^2} + \sqrt{\left( \frac{1}{2} - r \frac{c_s^2}{1+c_s^2} \right)^2 + (1-r)r \left( \frac{c_s^2}{1+c_s^2} \right)^2} \right] \quad (20)$$

$$\gamma^2 = \frac{1}{1-r} \left( \frac{1}{2} - r \frac{c_s^2}{1+c_s^2} + \sqrt{\frac{1}{4} - r \frac{c_s^2}{(1+c_s^2)^2}} \right) \quad (21)$$

which agrees with Eq. (14) for  $c_s^2 = 1/3$  and  $\gamma^2 = 1/(1-r)$  for  $c_s^2 = 0$ . Here,  $r$  plays the role of the square of a pseudo-velocity, so we could rename  $r \rightarrow v^2$ , so then

$$\gamma^2 = \frac{1}{1-v^2} \left( \frac{1}{2} - v^2 \frac{c_s^2}{1+c_s^2} + \sqrt{\frac{1}{4} - v^2 \frac{c_s^2}{(1+c_s^2)^2}} \right) \quad (22)$$

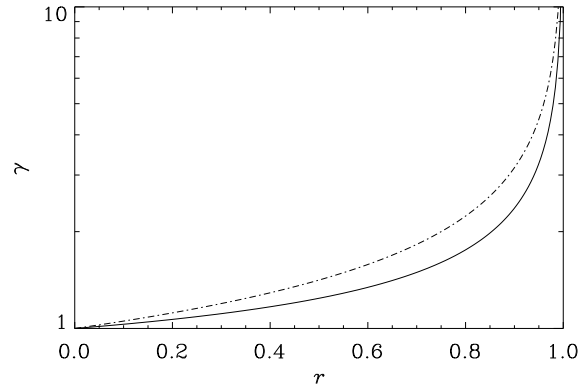


Figure 1:  $\gamma$  versus  $r$ . Solid line for  $c_s^2 = 1/3$  and dashed-dotted line for  $c_s = 0$ .

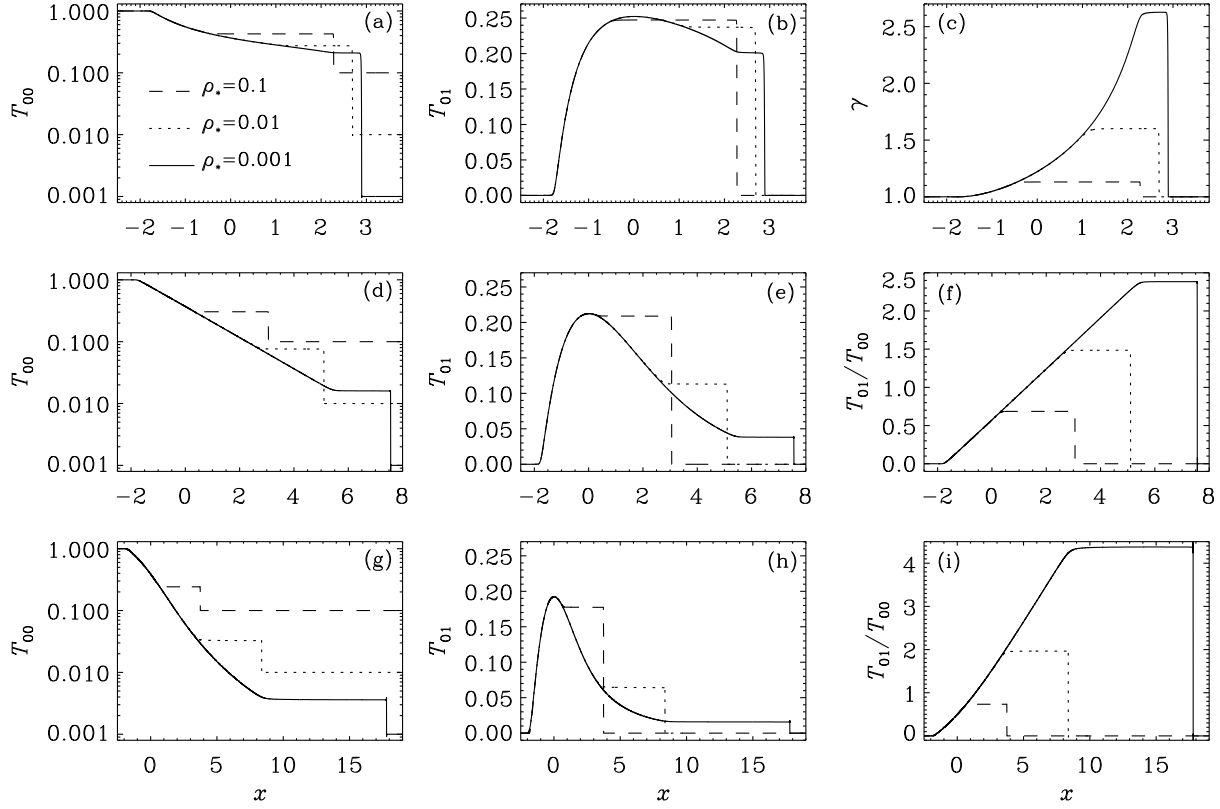


Figure 2: Shock tube tests for (a)–(c) the relativistic case, (d)–(f) the nonrelativistic case with isothermal equation of state, and (g)–(i) the nonrelativistic case with ultrarelativistic equation of state.

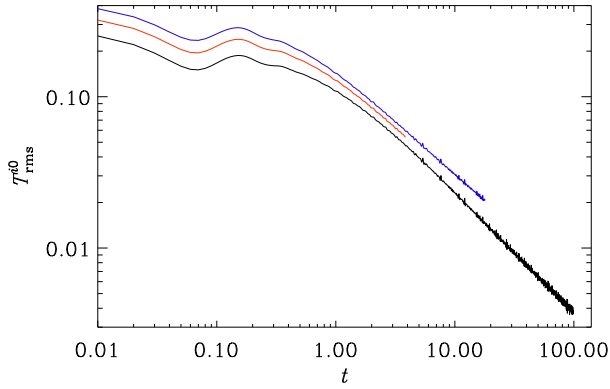


Figure 3: 2-D decaying turbulence for Runs A, B, and D.

### 3 Computation of $T^{ij}$

To compute  $T^{ij}$ , we use  $T^{0i}$  and  $T^{00}$ . We use Eq. (4) and  $\rho/3 = T^{00}/(4\gamma^2 - 1)$  to write

$$T^{ij} = \left(1 - \frac{1}{4\gamma^2}\right) \frac{T^{0i}T^{0j}}{T^{00}} + \frac{T^{00}}{4\gamma^2 - 1} \delta_{ij} \quad (23)$$

### 4 Magnetic runs

In the momentum equation, the Reynolds/Maxwell tensor is

$$T^{ij} = \frac{4}{3}\rho\gamma^2 u_i u_j + \frac{1}{3}\rho\delta_{ij} - B_i B_j + \frac{1}{2}B^2\delta_{ij} \quad (24)$$

We set  $\mathbf{E} = -\mathbf{u} \times \mathbf{B} + \eta \mathbf{J}$  and neglect term of  $O(\mathbf{E}^2) \ll O(\mathbf{B}^2)$ . Furthermore, the divergence of the magnetic part of  $T^{ij}$  is just  $\mathbf{J} \times \mathbf{B}$ . It is therefore convenient to solve

$$T^{00}_{,0} = -T^{0i}_{,i} \quad (25)$$

$$T^{i0}_{,0} = -{}^H T^{ij}_{,j} \quad (26)$$

where  ${}^H T^{ij}$  is the hydro stress given by Eq. (4). The other components of the stress,  $T^{00}$  and  $T^{i0}$ , however, do contain the magnetic field. In particular, we have

$$T^{00} = \frac{4}{3}\rho\gamma^2 - \frac{1}{3}\rho + \frac{1}{2}B^2 \quad (27)$$

$$T^{0j} = \frac{4}{3}\rho\gamma^2 u_j + (\mathbf{E} \times \mathbf{B})_j \quad (28)$$

Table 1: Parameters used for the 1-D shock tube tests.

Case	$\delta x$	$\delta t$	$\nu$	$\mu$	$\gamma_{\max}$	$u_{\max}$
Relativistic	$1.5 \times 10^{-3}$	$2 \times 10^{-4}$	$2 \times 10^{-4}$	$1 \times 10^{-4}$	1.13	0.47
	$1.5 \times 10^{-3}$	$2 \times 10^{-4}$	$2 \times 10^{-4}$	$1 \times 10^{-4}$	1.60	0.78
	$1.5 \times 10^{-3}$	$2 \times 10^{-4}$	$2 \times 10^{-4}$	$1 \times 10^{-4}$	2.63	0.92
Non-relativ.	$1.5 \times 10^{-3}$	$2 \times 10^{-4}$	$5 \times 10^{-4}$	$1 \times 10^{-4}$	1.37	0.69
	$1.6 \times 10^{-3}$	$2 \times 10^{-4}$	$5 \times 10^{-4}$	$2 \times 10^{-4}$	–	1.49
	$2.2 \times 10^{-3}$	$2 \times 10^{-4}$	$5 \times 10^{-4}$	$2 \times 10^{-4}$	–	2.38
Relativ. EoS	$1.5 \times 10^{-3}$	$2 \times 10^{-4}$	$1 \times 10^{-3}$	$1 \times 10^{-4}$	1.20	0.55
	$2.7 \times 10^{-3}$	$1 \times 10^{-4}$	$2 \times 10^{-3}$	$1 \times 10^{-3}$	–	1.47
	$2.7 \times 10^{-3}$	$1 \times 10^{-4}$	$2 \times 10^{-3}$	$1 \times 10^{-3}$	–	3.28

Table 2: Parameters used for 2-D turbulence tests.  
 $q_{\text{irro}} = 1$  (irrotational case).

Run	$A$	$u_{\text{rms}}$
A	1.5	4.2771E-01
B	1.2	3.6165E-01
C	1.0	3.1199E-01
D	0.9	2.8539E-01

Here, ignoring the resistive term  $\eta \mathbf{J} \times \mathbf{B}$  for now, the Poynting flux can also be written as

$$\mathbf{E} \times \mathbf{B} = (\mathbf{B}^2 \delta_{ij} - B_i B_j) u_j \quad (29)$$

Therefore

$$T^{0i} = \left[ \left( \frac{4}{3} \rho \gamma^2 + \mathbf{B}^2 \right) \delta_{ij} - B_i B_j \right] u_j \quad (30)$$

$$(T^{0i})^2 = D^2 \mathbf{u}^2 - (2D - \mathbf{B}^2) (\mathbf{u} \cdot \mathbf{B})^2 \quad (31)$$

where  $D = \frac{4}{3} \rho \gamma^2 + \mathbf{B}^2$ . To calculate  $r = v^2$ , we use iteration:

$$v^2 = \frac{(T^{0i})^2 + (2D - \mathbf{B}^2) (\mathbf{u} \cdot \mathbf{B})^2}{(T^{00} - \frac{1}{2} \mathbf{B}^2)^2} \quad (32)$$

or

$$v^2 = \frac{(T^{0i})^2 + \left( \frac{8}{3} \rho \gamma^2 + \mathbf{B}^2 \right) (\mathbf{u} \cdot \mathbf{B})^2}{(T^{00} - \frac{1}{2} \mathbf{B}^2)^2} \quad (33)$$

Assume for now  $\mathbf{u} \cdot \mathbf{B} = 0$ , so

$$v^2 = \frac{(T^{0i})^2}{(T^{00} - \frac{1}{2} \mathbf{B}^2)^2} = \frac{D^2 \mathbf{u}^2}{(T^{00} - \frac{1}{2} \mathbf{B}^2)^2} \quad (34)$$

Thus, replacing  $T^{00} - \frac{1}{2} \mathbf{B}^2 = \frac{4}{3} \rho \gamma^2 (1 - 1/4 \gamma^2)$ ,

$$v^2 = \frac{(\frac{4}{3} \rho \gamma^2 + \mathbf{B}^2)^2 (1 - 1/\gamma^2)}{(\frac{4}{3} \rho \gamma^2)^2 (1 - 1/4 \gamma^2)^2} \quad (35)$$

so

$$v^2 = \left( 1 + \frac{\mathbf{B}^2}{\frac{4}{3} \rho \gamma^2} \right)^2 \frac{(1 - 1/\gamma^2)}{(1 - 1/4 \gamma^2)^2} \quad (36)$$

or

$$v^2 = \left( 1 + \frac{\mathbf{B}^2}{\frac{4}{3} \rho \gamma^2} \right)^2 \frac{\gamma^2 (\gamma^2 - 1)}{(\gamma^2 - 1/4)^2} \quad (37)$$

so in the magnetic case, where  $v^2$  is given by Eq. (33), we have to replace in Eq. (22)

$$v^2 \rightarrow v^2 / [1 + (v_{\text{A}}^{\text{rel}})^2]^2. \quad (38)$$

where  $(v_{\text{A}}^{\text{rel}})^2 = \mathbf{B}^2 / (\frac{4}{3} \rho \gamma^2)$  is the pseudo Alfvén speed. (It is also not a non-relativistic one, because it contains  $\gamma$ .)

## 5 Calculation of $u_i$ and hydro stress for $T^{ij}$

Once we have  $\gamma^2$ , we can compute  $\mathbf{u}$  (here for, for Alfvén waves, we have  $\mathbf{u} \cdot \mathbf{B} = 0$ ) using Eq. (30),

$$u_i = \frac{T^{0i}}{\frac{4}{3} \rho \gamma^2 + \mathbf{B}^2} \quad (39)$$

or, in terms of  $T^{00}$ , using

$$\frac{4}{3} \rho \gamma^2 = \frac{T^{00} - \frac{1}{2} \mathbf{B}^2}{1 - \frac{1}{4 \gamma^2}}, \quad (40)$$

we have

$$u_i = \frac{T^{0i}}{\frac{T^{00} - \frac{1}{2} \mathbf{B}^2}{1 - 1/4 \gamma^2} + \mathbf{B}^2} \quad (41)$$

which is the expression used currently in the code.  
By expanding it, it can also be written as

$$u_i = \frac{T^{0i}(1 - 1/4\gamma^2)}{T^{00} - \frac{1}{2}\mathbf{B}^2 + (1 - 1/4\gamma^2)\mathbf{B}^2} \quad (42)$$

to get

$$u_i = \frac{T^{0i}(1 - 1/4\gamma^2)}{T^{00} + (1 - 1/2\gamma^2)\mathbf{B}^2/2} \quad (43)$$

To compute  ${}^{\text{H}}T^{ij}$ , we again use  $T^{0i}$  and  $T^{00}$ . We use Eq. (4) and  $\rho/3 = (T^{00} - \frac{1}{2}\mathbf{B}^2)/(4\gamma^2 - 1)$  to write

$$T^{ij} = \frac{T^{0i}T^{0j}}{(T^{00} - \frac{1}{2}\mathbf{B}^2)/(1 - 1/4\gamma^2) + \mathbf{B}^2} + \frac{T^{00} - \frac{1}{2}\mathbf{B}^2}{4\gamma^2 - 1}\delta_{ij} \quad (44)$$

where

$$\frac{4}{3}\rho\gamma^2 = \frac{T^{00} - \frac{1}{2}\mathbf{B}^2}{1 - 1/4\gamma^2} \quad (45)$$

and

$$\frac{1}{3}\rho = \frac{T^{00} - \frac{1}{2}\mathbf{B}^2}{4\gamma^2 - 1} \quad (46)$$

and therefore more compactly

$$T^{ij} = \frac{T^{0i}T^{0j}}{\frac{4}{3}\rho\gamma^2 + \mathbf{B}^2} + \frac{1}{3}\rho\delta_{ij} \quad (47)$$

In terms of  $c_s$  etc, we have

$$\rho = \frac{T^{00} - \frac{1}{2}\mathbf{B}^2}{(1 + c_s^2)\gamma^2 - c_s^2} \quad (48)$$

and

$$\frac{1}{1 - 1/4\gamma^2} \rightarrow \frac{1}{1 - c_s^2/[\gamma^2(1 + c_s^2)]} \quad (49)$$

or

$$\frac{1}{1 - 1/4\gamma^2} \rightarrow \frac{(1 + c_s^2)\gamma^2}{(1 + c_s^2)\gamma^2 - c_s^2} \quad (50)$$